

# Analysis of Concentration Dependencies for an Optical Directional Coupler Design

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**Abstract**—An integrated directional coupler is designed for a bidirectional communication on a single waveguide by separating both data streams within individual branches. Thereby, an adjustment of the numerical aperture of the transmitting branch is a promising optimization approach. As the couplers are manufactured by a field-assisted diffusion process the numerical aperture is directly related to the exchange ion concentration. The efficiency of the designed coupler and its optimization approaches is calculated with a geometrical optics algorithm.

## I. INTRODUCTION

Optical intra-board links have been figured out as promising technology for future board level communication [1]. Integrated optical waveguides and devices are manufactured with a field-assisted diffusion process within thin glass sheets, which can be embedded as optical layers in conventional printed circuit boards [2]. Since space is limited at board level applications, a bidirectional communication on a single waveguide is required. Therefore, a directional coupler manufactured with a field assisted ion-exchange process is designed which realizes a separation of both transmission directions [3], [4].

## II. DIRECTIONAL COUPLER DESIGN AND OPTIMIZATION

The directional coupler, which is designed for simultaneous bidirectional communication on a single waveguide, has the basic idea of extracting both signal directions by separating them into two individual branches. Therefore, a mask structure for a field-assisted ion exchange with different optimization approaches is investigated. As illustrated in Figure 1 the directional coupler consists of an S-bend which guides the received signals to the optical receiver and a straight waveguide branching that works as a transmitting branch.

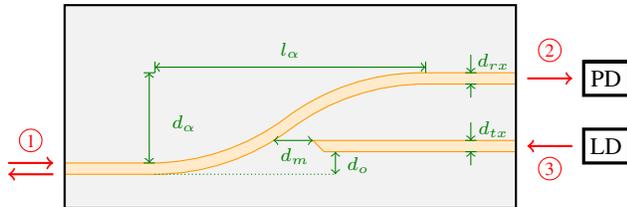


Fig. 1. Mask design of an S-bend with a branching and the optimization approaches of mask bridge  $d_m$ , coupling angle  $\alpha$  and mask opening width of the transmitting branch  $d_{tx}$ .

The efficiency  $\eta$  of the designed couplers is determined by the forced losses in both transmission directions

$$\eta = \eta_{rx} \cdot \eta_{tx}. \quad (1)$$

Therefore different approaches to minimize damping are investigated. A mask bridge  $d_m$  between both branches, an offset  $d_o$  of the transmitting branch and the coupling angle  $\alpha = \arctan(d_\alpha/l_\alpha)$  have already been characterized as promising optimization techniques in the previous works [3] and [5]. The exchange ion concentration  $c$ , that is related to the mask opening width  $d_{tx}$  as shown in Figure 2, is an additional promising technique to increase the efficiency of the designed coupler. Since the exchange ion concentration  $c$  is directly related to the refractive index [6]

$$n_s(\vec{r}) = n_{sub} + \Delta n_{ex} \cdot c(\vec{r}), \quad (2)$$

the numerical aperture of the transmitting branch can be modeled by a variation of  $d_{tx}$ .

## III. MATHEMATICAL METHODS

For the investigation of concentration dependencies on the efficiency of the designed directional coupler's the field-assisted ion exchange is modeled by solving the continuity equation for the ionic flux [7]

$$\frac{\partial c}{\partial t} = \frac{D}{1 - \alpha c} \left( \Delta c + \frac{\alpha (\nabla c)^2}{1 - \alpha c} - \frac{q\vec{E}}{kT} \nabla c \right) \quad (3)$$

with the finite-element-method. The geometrical dimensions of the manufactured waveguides are thereby mainly depending on the chosen process parameters of diffusion time  $t$ , electrical field strength  $E$  and process temperature  $T$ . The designed

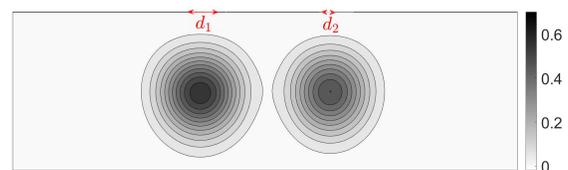


Fig. 2. Cross section of two waveguides manufactured with a field-assisted ion exchange from different mask opening widths  $d_1$  and  $d_2$ .

coupler, presented in this work, is modeled as a highly multimodal waveguide with large geometrical dimensions compared to the optical wavelength. For this reason, a geometrical optics algorithm solving the ray equation

$$\frac{d}{ds} \left( n \frac{dr}{ds} \right) = \nabla n(r) \quad (4)$$

is used as an efficient method for the loss calculation [8]. The ray extinction is thereby modeled as a gaussian pulse [9].

#### IV. INVESTIGATION SERIES AND CALCULATED RESULTS

For the purpose of optimizing the efficiency of the structure several approaches have been mentioned before. The mask bridge  $d_m$  which is modeled from  $0\mu m$  to  $500\mu m$  should realize a decoupling of both branches. For the bend angle  $\alpha = 5^\circ$  is applied. Thereby,  $\alpha$  mainly influences the losses in receiving direction [10]. For the investigation of concentration dependencies of the designed coupler the mask opening width  $d_{tx}$  of the transmitting branch is varied in a range of  $1\mu m$  to  $3\mu m$ . This leads to a smaller numerical apertures of the transmitting that should increase the efficiency in receiving direction. The transmitting branch offsets are varied from  $0\mu m$  to  $20\mu m$ . In Figure 3, the calculated efficiencies are visualized in both directions, wherein the receiving direction is continuously represented and the transmitting direction is dashed. Figure 3 shows that smaller mask openings  $d_s$  of the transmitting branch lead to higher efficiencies, especially in sending direction (TX) for small offsets  $d_o$ . For larger offsets  $d_o$ , the effect of mask opening width  $d_{tx}$  decreases because the efficiencies converge faster against their final value for increasing mask bridges  $d_s$ . From a multiplication of the curves in both directions the overall efficiency  $\eta$  can be derived which is shown in Figure 4. By reducing the mask opening width  $d_{tx}$  of the transmitting branch, an increase of the overall efficiency can be achieved for larger offsets  $d_o$ . A maximum overall efficiency of 67.4% can be achieved with a mask opening width of  $d_{tx} = 1\mu m$  compared to 61.3% which has been the maximum efficiency in further investigations [3].

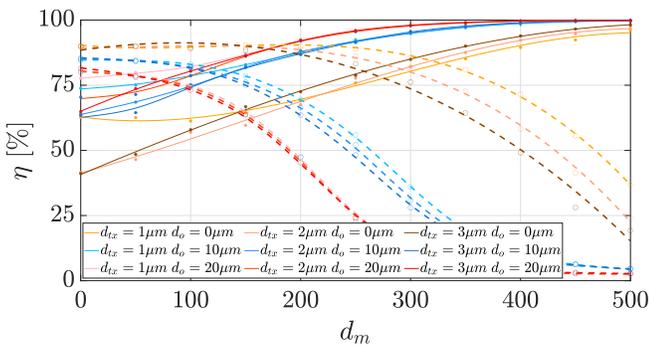


Fig. 3. Calculated efficiencies in receiving direction (RX,continuous) and transmitting direction (TX,dashed) that is depending on various optimization parameters.

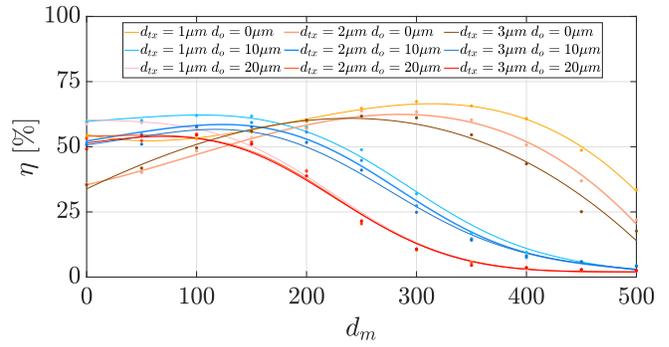


Fig. 4. Calculated overall efficiency  $\eta$  that is derived by a multiplication of the efficiencies  $\eta_{rx}$  and  $\eta_{tx}$  in both directions.

#### V. CONCLUSION

In this work a promising optimization approach for an integrated directional coupler which is manufactured by a field-assisted ion-exchange is presented. By reducing the mask opening width  $d_{tx}$  of the transmitting branch, the overall efficiency can be increased by 6.1% compared to previous results [3]. The numerical aperture of the transmitting branch is thereby adjusted by the mask opening width  $d_{tx}$ . This requires for further investigations a quantitative analysis of the refractive index profiles for different mask opening widths and a verification of the calculated results by measurements to evolve an optimized directional coupler structure.

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