

A new Technique for Simulating Semiconductor Laser Resonators

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NUSOD conference, September 1st, 2008



Outline

1 Challenge

2 Simulation Technique

3 Simulation Results



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2 Simulation Technique

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Goal

Optimal Laser

Good beam quality ↔ High output power ↔ Stabilized wavelength

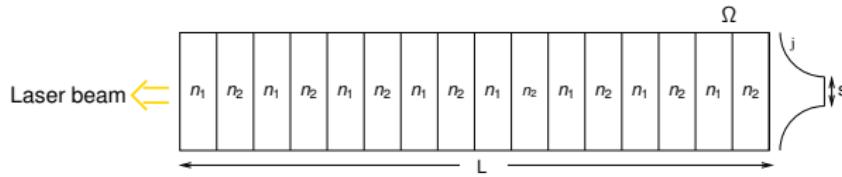
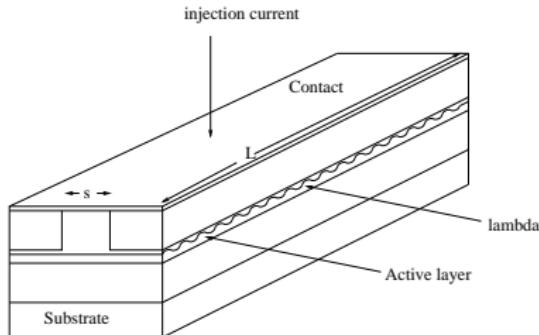
Understanding of the **influence** of different parameters on the dynamics in the laser device

→ **Simulation of the laser device**



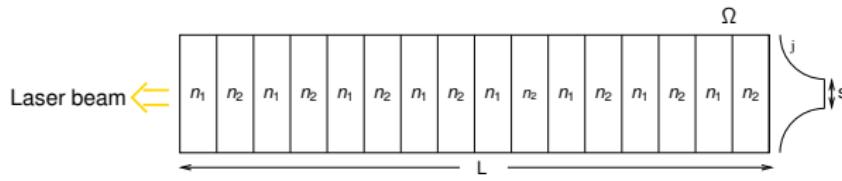
Distributed Feedback Laser

- **Long** resonator with length L
- **Small** stripe width of size s of injection current j
- Layers with different refractive indices (gratings) → **Internal reflections** of the optical wave



Difficulties in the simulation of the optical wave

- Large-scale simulations of the wave equation require a **large number of grid points**
- Internal reflections → **Propagation** in forward and backward direction has to be treated **simultaneously**



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Usual Approaches

Well-known methods for the simulation of optical waves

- Beam Propagation Method
- Finite Difference Time Domain Method
- Finite Element Method (FEM) with standard Finite Elements

But: Internal reflections and large resonators **cannot** be simulated by these methods

$\xrightarrow{1D}$ Transfer Matrix Method (TMM)

But: Tapered lasers need a **2D**-simulation



Idea

Trigonometric Finite Wave Elements (TFWE)

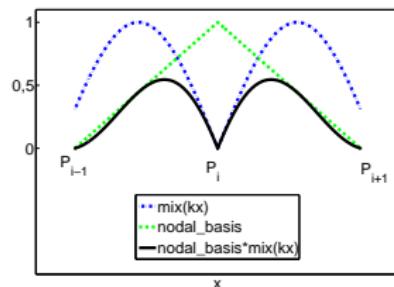
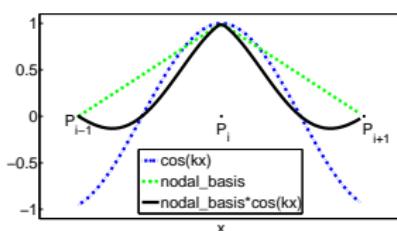
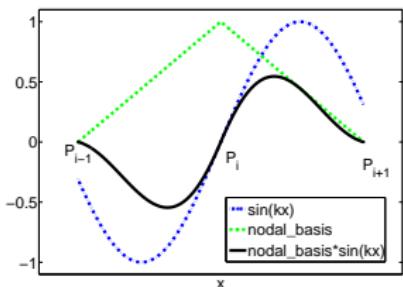
- Special Finite Elements
- Provide the same solution as the **TMM** for 1D Helmholtz equation
- Extendable to **higher dimensions**
- Extendable to **time-dynamic** problems

→ **TFWE method combines advantages of TMM and FEM**



Trigonometric Finite Wave Elements in 1D

1D linear nodal basis functions are multiplied by appropriate **sine** and **cosine** functions



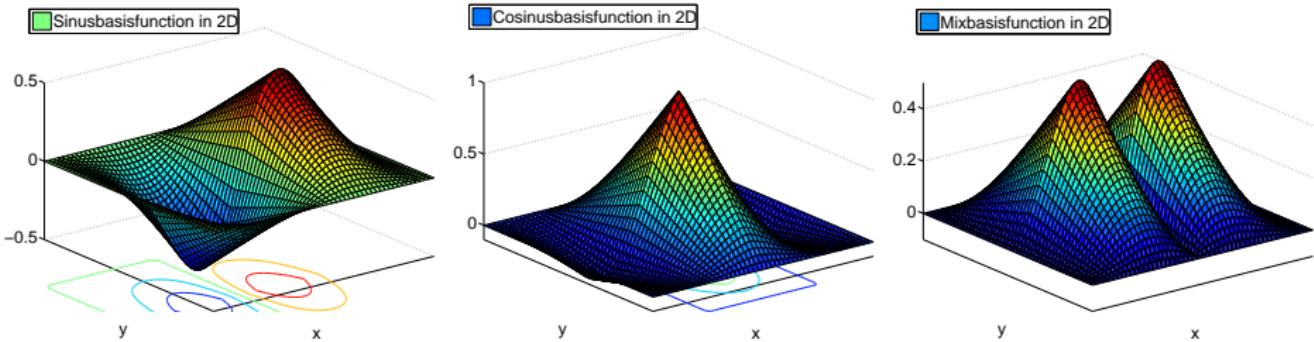
These 3 basis functions per node span the Finite Element space V_h .

k : wave number



Trigonometric Finite Wave Elements in 2D

Construct TFWE in **2D** by a tensor product of 1D TFWE in propagation direction and linear nodal basis functions in perpendicular direction

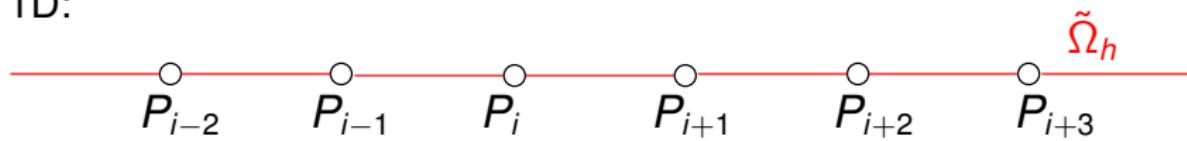


Oscillation Assumption

Oscillation Assumption

Let $u \in H^2(\Omega) \cap C(\Omega)$ **oscillate** with an approximate local wave number k . This means, that $u = u^+ \exp(i k x) + u^- \exp(-i k x)$, where $u^+ \exp(i k x) \in H^2(\tilde{\Omega}_h)$, $u^- \exp(-i k x) \in H^2(\tilde{\Omega}_h)$, $\|u_{xx}^+\|_{L^2(\tilde{\Omega}_h)} \ll \|u_{xx}\|_{L^2(\Omega)}$, and $\|u_{xx}^-\|_{L^2(\tilde{\Omega}_h)} \ll \|u_{xx}\|_{L^2(\Omega)}$.

1D:



1D: $\tilde{\Omega}_h$: Ω without grid points

$$u_{xx} := \frac{d^2 u}{dx^2}$$

$\tilde{\Omega}_h$: Ω without grid lines

$$u_{xx} := \frac{\partial^2 u}{\partial x^2}$$



Approximation property of TFWE

Oscillation Assumption

Let $u \in H^2(\Omega) \cap \mathcal{C}(\Omega)$ **oscillate** with local wave number k .

Theorem

Let $u \in H^2(\Omega)$ satisfy the Oscillation Assumption. Then,

$$\|u - I_h^{osc}(u)\|_{H^1(\Omega)} \leq C\mathbf{h}(k_{max}\mathbf{h} + 1) \left(\|u^+\|_{H^2(\tilde{\Omega}_h)} + \|u^-\|_{H^2(\tilde{\Omega}_h)} \right)$$

where C can be chosen **independently** of \mathbf{h} and k_{max} , if \mathbf{h} , $|k|_{H^{1,\infty}(\tilde{\Omega}_h)}$, and $|k|_{H^{2,\infty}(\tilde{\Omega}_h)}$ are bounded from above.

1D: $k_{max} := \max_{1 \leq j \leq N} |k_j|$

k_j : discretized wave numbers

N : number of grid points

$\mathbf{h} := h$

$I_h^{osc} : H^2(\Omega) \longrightarrow V_h$: interpolation operator, V_h : TFWE space

2D: $k_{max} := \max_{1 \leq j \leq N_y} \max_{1 \leq i \leq N_x} |k_{ij}|$

k_{ij} : discretized wave numbers

N_x, N_y : number of grid points

$\mathbf{h} := \max\{h_x, h_y\}$



Approximation property of standard Finite Elements

Oscillation Assumption

Let $u \in H^2(\Omega) \cap C(\Omega)$ **oscillate** with local wave number k .

Theorem

Let $u \in H^2(\Omega)$ satisfy the Oscillation Assumption. Then, we have

$$\|u - I_h(u)\|_{H^1(\Omega)} \leq Ch(k_{max} + 1)^2 (\|u^+\|_{H^2(\tilde{\Omega}_h)} + \|u^-\|_{H^2(\tilde{\Omega}_h)})$$

where C can be chosen **independently** of h and k_{max} , if h , $|k|_{H^{1,\infty}(\tilde{\Omega}_h)}$, and $|k|_{H^{2,\infty}(\tilde{\Omega}_h)}$ are bounded from above.

1D: $I_h : H^2(\Omega) \longrightarrow V_h^{lin}$: linear interpolation operator

V_h^{lin} : linear FE space

2D: $I_h : H^2(\Omega) \longrightarrow V_h^{bilinear}$: bilinear interpolation operator

$V_h^{bilinear}$: bilinear FE space



Conclusion

Conclusion

Increasing wave number k_{max} , assuming $\hbar k_{max} < C$:

- The upper bound for the approximation error for standard FE **increases** with k_{max}^2
- The upper bound for the approximation error for TFWE keeps **constant**

Remark

The assumption $\hbar k_{max} < C$ is true in most applications, e.g. in computational optics one has $\hbar < \tilde{C}\lambda = \tilde{C}\frac{2\pi}{k}$.

λ : wavelength of the considered optical wave
 $C, \tilde{C} > 0$: constants independent of \hbar and k



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System of Coupled Partial Differential Equations

- Behavior of wave \tilde{E} is described by the wave equation; assuming $\tilde{E}(x, t) = \mathbf{E}(x, t) \exp(i\omega t)$ leads to

$$2i \frac{\bar{k}(\mathbf{n}_A)}{v_g} \frac{\partial \mathbf{E}}{\partial t} = \Delta \mathbf{E} + k^2(\mathbf{n}_A) \mathbf{E}$$

- Drift-diffusion equations determine the time-dynamic behavior of the carrier densities \mathbf{n}_A and \mathbf{n}_B

$$\frac{\partial \mathbf{n}_A}{\partial t} = \nabla(D_A \nabla \mathbf{n}_A) + C_1 \mathbf{n}_B - C_2 \mathbf{n}_A - r_{rec,A}(|\mathbf{E}|^2, \mathbf{n}_A) \quad \text{and}$$

$$\frac{\partial \mathbf{n}_B}{\partial t} = \nabla(D_B \nabla \mathbf{n}_B) + \tilde{C}_0 \mathbf{j} - \tilde{C}_1 \mathbf{n}_B + \tilde{C}_2 \mathbf{n}_A - r_{rec,B}$$

D_A, D_B : ambipolar diffusion constants, j : current density, v_g : group velocity, $r_{rec,A}, r_{rec,B}$: recombination densities

System of Coupled Partial Differential Equations

$$r_{rec,A} = A_A \mathbf{n_A} + B_A \mathbf{n_A}^2 + C_A \mathbf{n_A}^3 + r_{stim},$$

$$r_{rec,B} = A_B \mathbf{n_B} + B_B \mathbf{n_B}^2,$$

$$r_{stim} = \frac{c}{n_g} g_{nonlin} n,$$

$$g_{nonlin} = \begin{cases} \frac{g_0}{1+\varepsilon n} \ln\left(\frac{\mathbf{n_A}}{n_{tr}}\right) & \text{if } |\mathbf{n_A}| \geq n_{tr} \\ \frac{g_0}{1+\varepsilon n} \left(\frac{\mathbf{n_A}}{n_{tr}} - 1\right) & \text{if } |\mathbf{n_A}| < n_{tr} \end{cases}$$

$$k = \frac{\omega n'}{c} + \color{red}{\alpha_H} \frac{g_{nonlin}}{2} + i \frac{g_{nonlin} - \alpha_0}{2}$$

$$n = \frac{\epsilon_0 n' n_g}{2\hbar\omega} |\tilde{E}|^2 = \frac{\epsilon_0 n' n_g}{2\hbar\omega} |\mathbf{E}|^2.$$

A_A, B_A, C_A, A_B, B_B : recombination coefficients, n_{tr} : transparency carrier density, α_H : Henry factor

g_0 : differential gain, ε : gain compression factor, α_0 : absorption

Absorbing Boundary Condition (PML)

- Wave is considered on domain $\Omega =]0, L[\times] - \frac{W}{2}, \frac{W}{2}[$
- Wave is emitted on left hand side (at $x = 0$) → **Absorbing boundary condition** $ik\mathbf{E}(0, y) = \frac{\partial \mathbf{E}}{\partial x}(0, y)$
- Absorbing boundary is simulated by **PML** →
 - Domain Ω is increased to $\tilde{\Omega} =]-\delta, L[\times] - \frac{W}{2}, \frac{W}{2}[$
 - Schrödinger equation is transformed to

$$2i\frac{\tilde{k}}{v_g}\frac{\partial \mathbf{E}}{\partial t} = \frac{\partial}{\partial x}\frac{k}{\tilde{k}}\frac{\partial E}{\partial x} + \frac{\tilde{k}}{k}\frac{\partial^2 E}{\partial y^2} + k\tilde{k}\mathbf{E}$$

$$\tilde{k} := k - i\sigma(x) := k_0\bar{n} - i\sigma(x)$$

$$\tilde{\bar{k}} := \bar{k} - i\sigma(x) := k_0\bar{n} - i\sigma(x)$$

$$\sigma(x) := \sigma_c \frac{x^2}{\delta^2} \text{ for } x < 0, \quad \sigma(x) := 0 \text{ for } x \geq 0$$

$$\sigma_c := \frac{3}{2\delta} \log(1/R_0)$$

$$R_0 := 10^{-4} \text{ theoretical reflexion coefficient}$$



Discretization

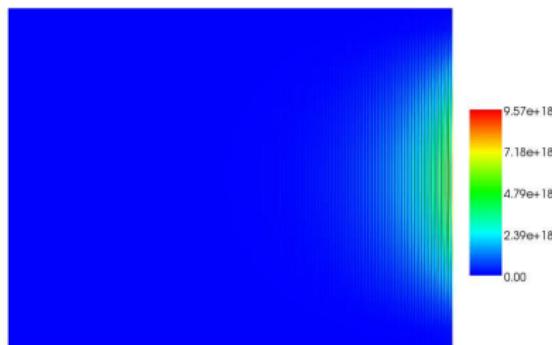
- **Spatial** discretization of the wave equation in propagation direction: at least one grid point per layer for resolving internal reflections
- **Temporal** discretization: wave with frequency
 $\omega \approx 1.935\text{GHz} \rightarrow \text{time step size } \tau \approx 0.3\text{ps} \rightarrow \omega\tau \approx 600.$

In the following examples: 840 layers, 841 grid points in propagation direction, 16/31 grid points in perpendicular direction, total simulation time: 4ns, current: 480mA, stripe width: $2.5\mu\text{m}$.

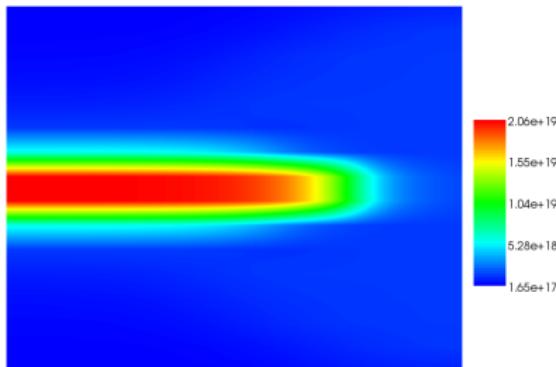


Photon and Carrier density ($\alpha_H = 0.0$)

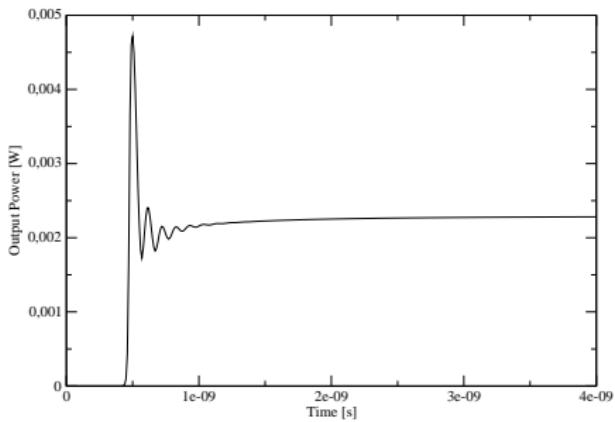
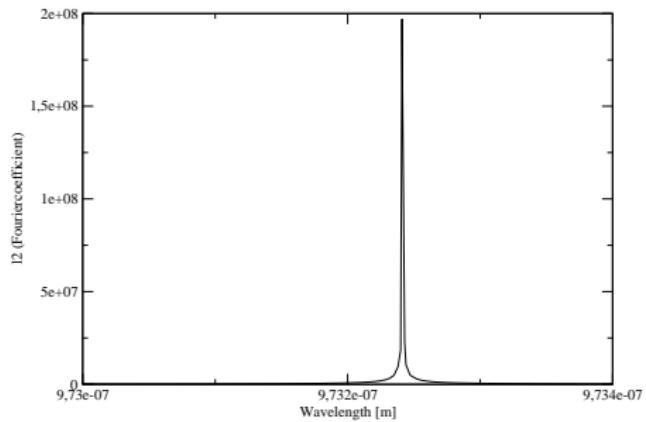
Photon density n



Carrier density n_A

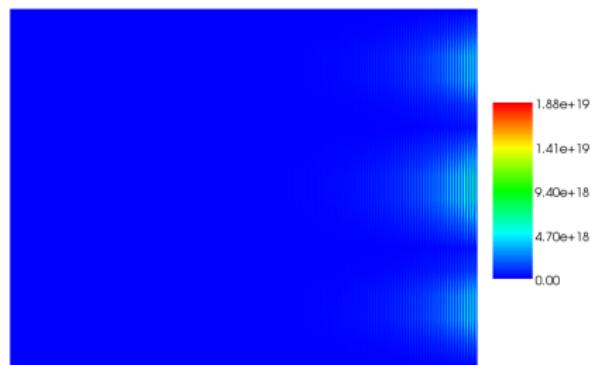


Frequency Spectrum and Output Power ($\alpha_H = 0.0$)

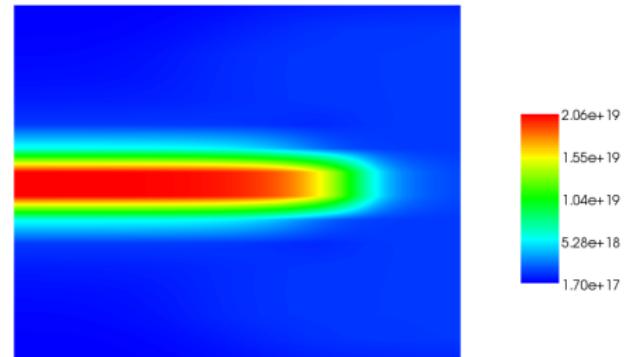


Photon and Carrier density ($\alpha_H = -0.5$)

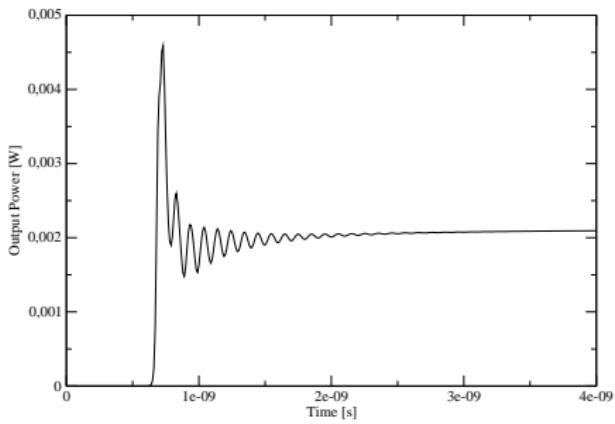
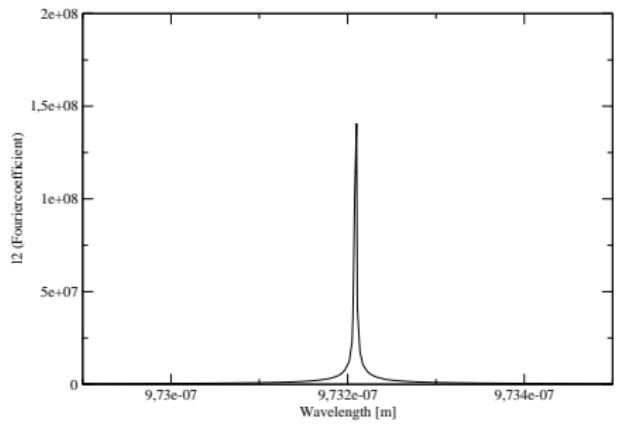
Photon density n



Carrier density n_A

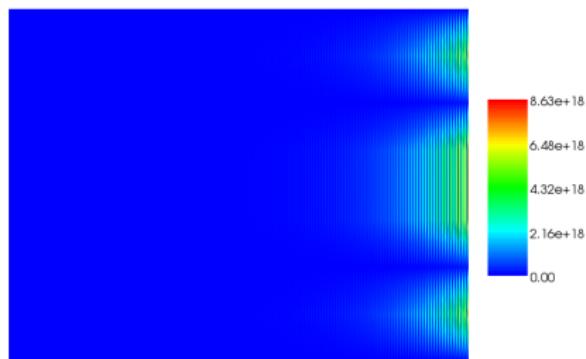


Frequency Spectrum and Output Power ($\alpha_H = -0.5$)

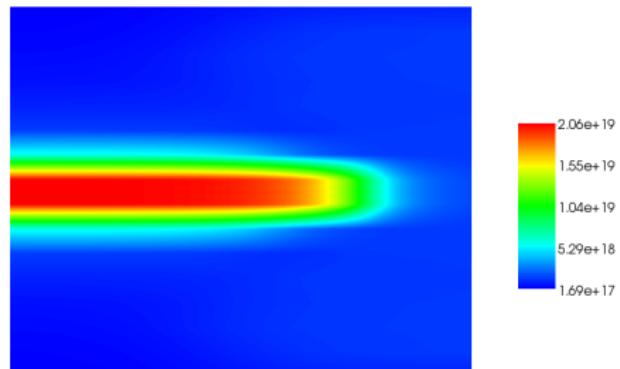


Photon and Carrier density ($\alpha_H = -2.5$)

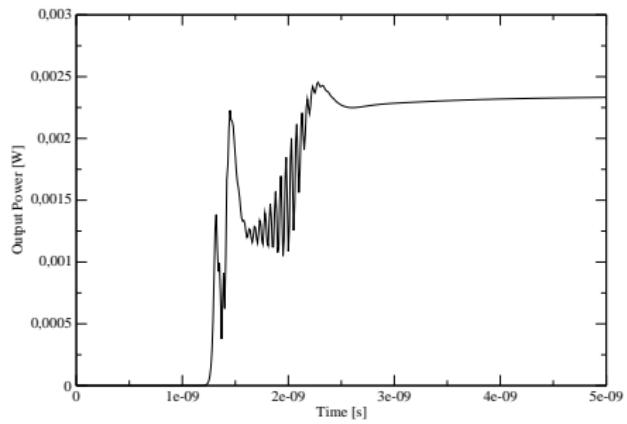
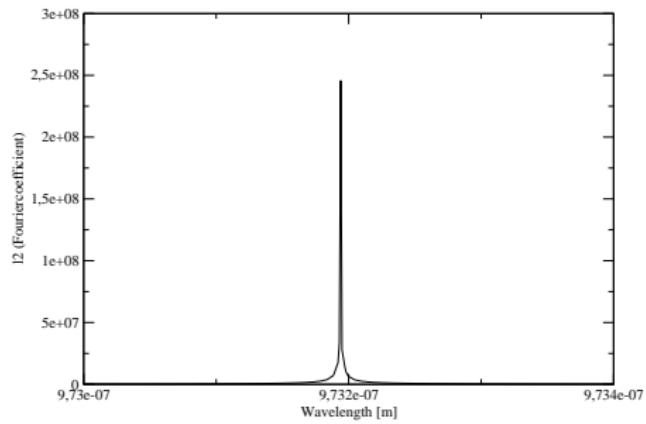
Photon density n



Carrier density n_A

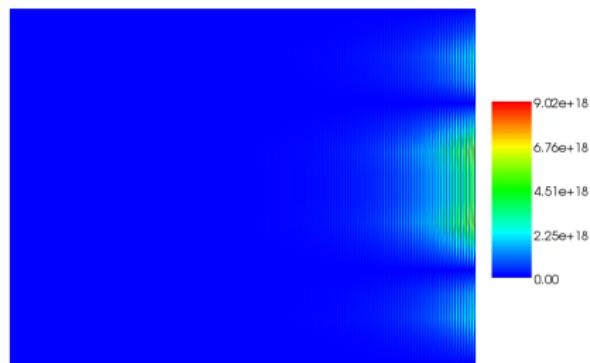


Frequency Spectrum and Output Power ($\alpha_H = -2.5$)

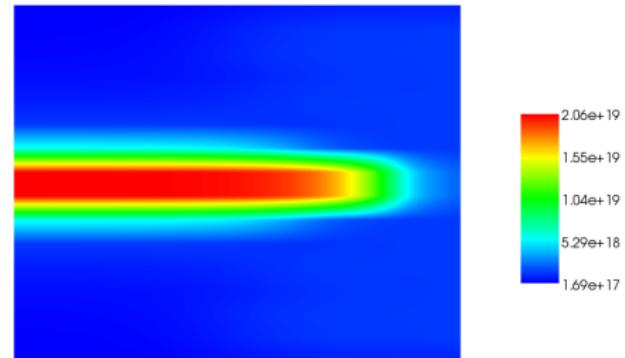


Photon and Carrier density ($\alpha_H = -3.0$)

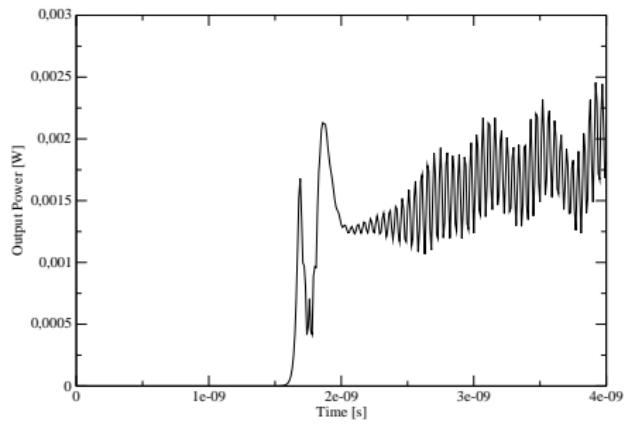
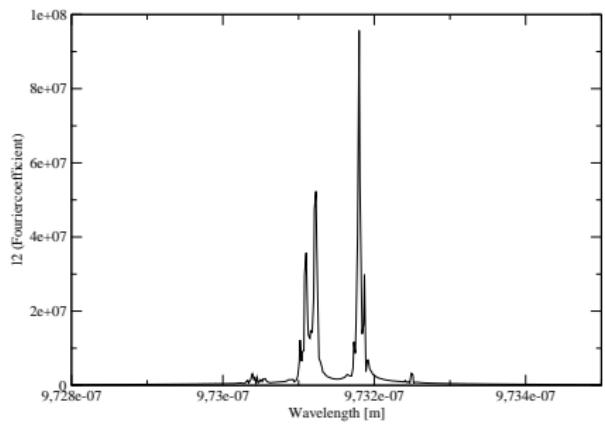
Photon density n



Carrier density n_A

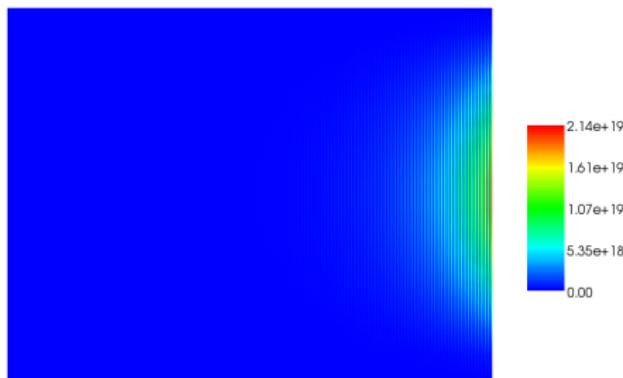


Frequency Spectrum and Output Power ($\alpha_H = -3.0$)

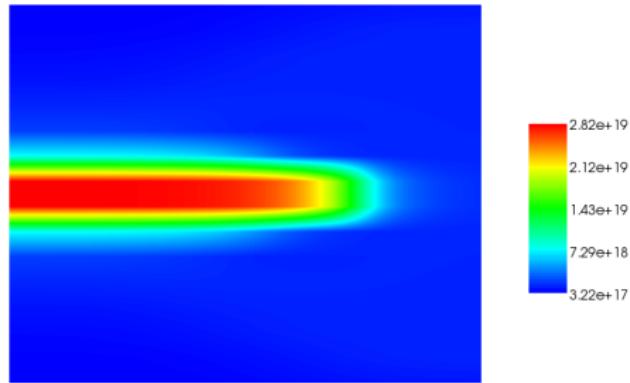


Photon and Carrier density ($\alpha_H = 0.0, I = 960mA$)

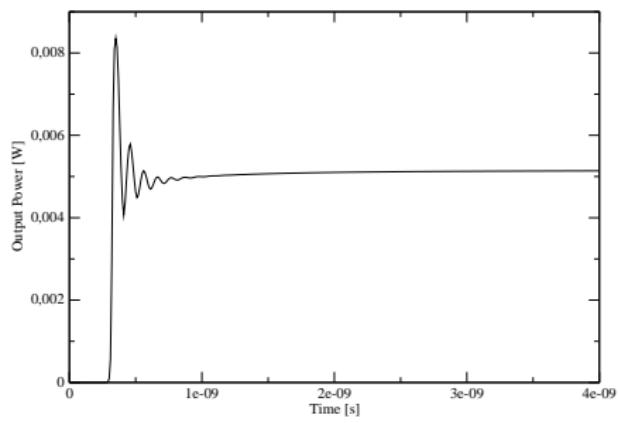
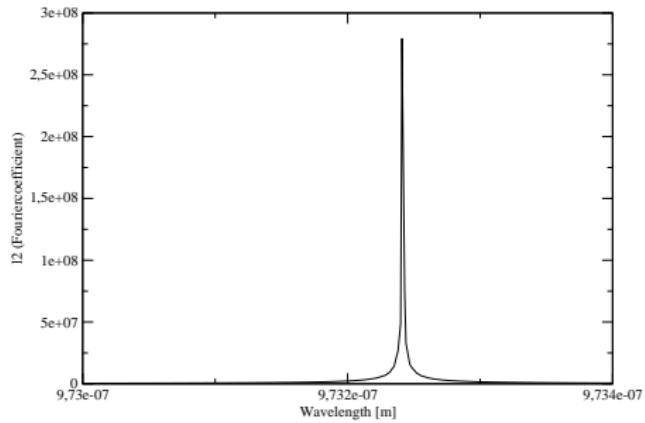
Photon density n



Carrier density n_A

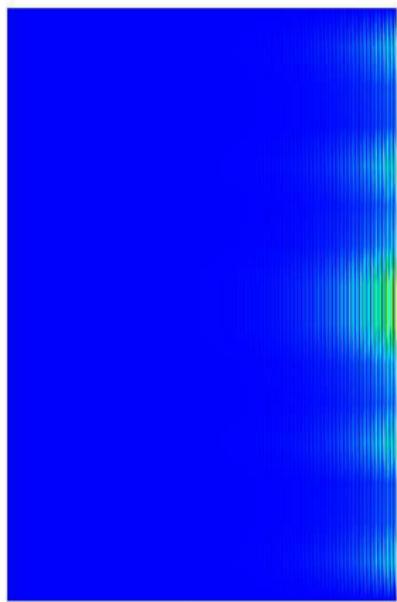


Frequency Spectrum and Output Power ($\alpha_H = 0.0$, $I = 960mA$)

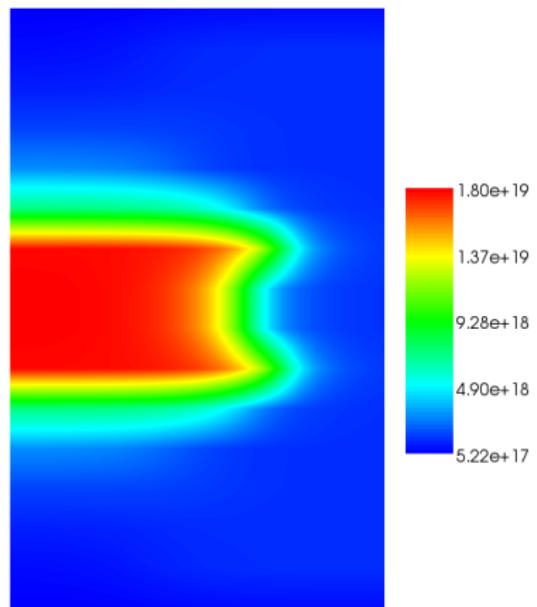


Photon and Carrier density ($\alpha_H = -2.0, s = 25\mu m$)

Photon density n

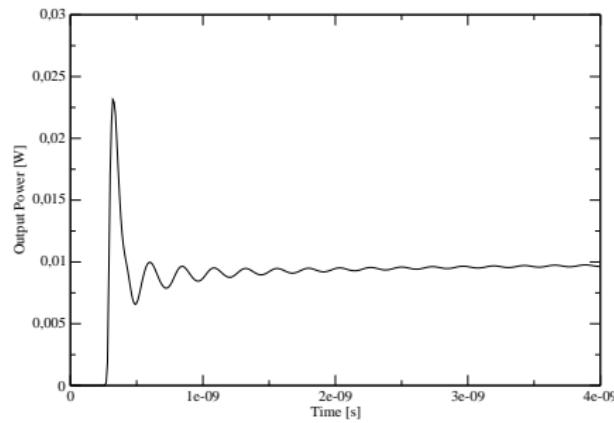
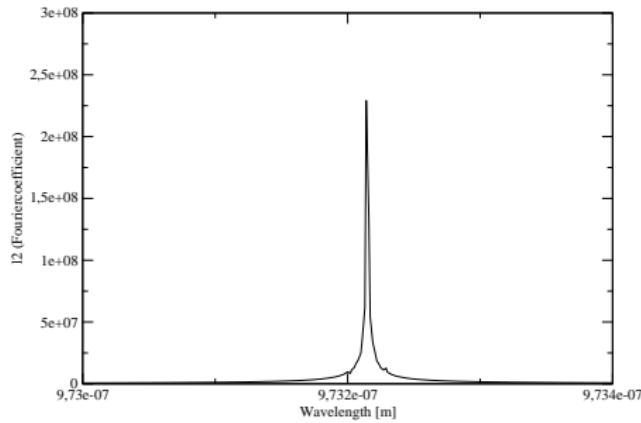


Carrier density n_A



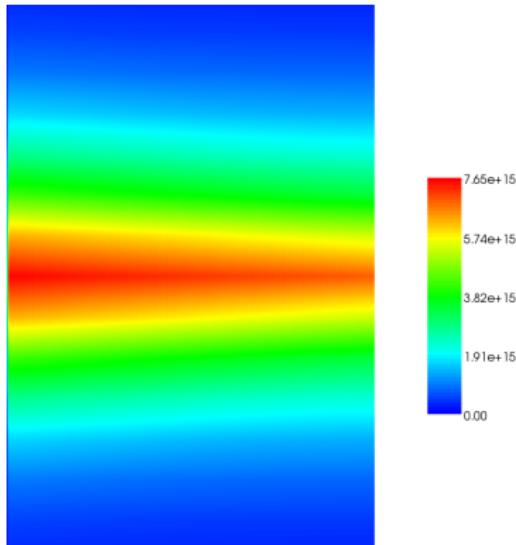
Frequency Spectrum and Output Power

($\alpha_H = -2.0$, $s = 25\mu m$)

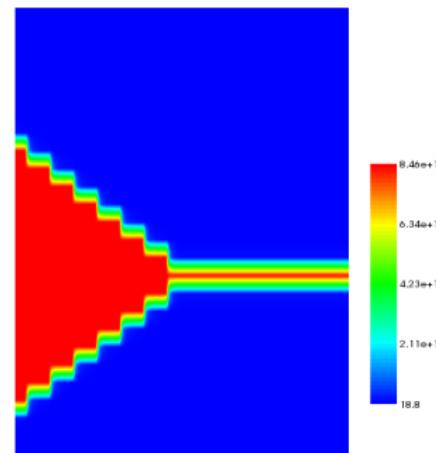


Tapering

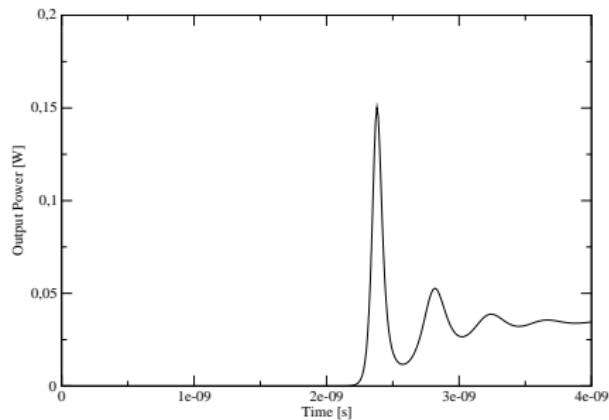
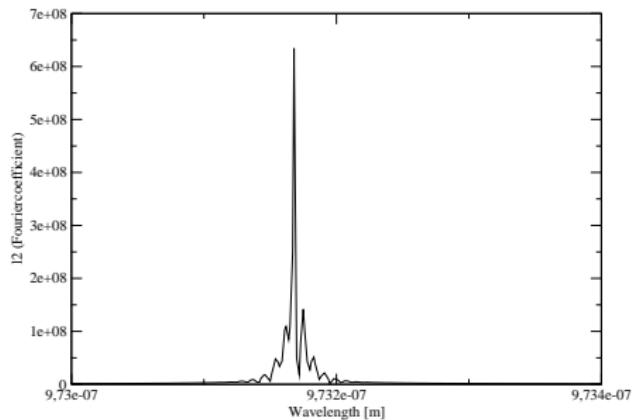
Zoom in photon density n



Carrier density n_A



Tapering



Summary

TFWE method combines advantages of FEM and TMM

- TFWE can be applied to time-periodic and **time-dynamic** wave problems
- **Internal reflections** can be simulated in 2D
- TFWE lead to better **performance** than standard FE

Simulation can support the tuning of DFB lasers

Influence of stripe width, current, Henry factor,... on the resulting mode, wavelength, and output power can be examined

Outlook

- Comparison: **Experiment ↔ Simulation**
- Simulation of **different** laser devices (disc lasers, three-section lasers,...)
- Extension of the simulation to **3D**
- Introduction of **multigrid** method for solving the wave equation

