



FDTD Modelling and Experimental Verification of FWM in Semiconductor Micro-Resonators

Masafumi Fujii*, [Christian Koos](#), Christopher Poulton**,
[Juerg Leuthold](#), [Wolfgang Freude](#)

*Institute for High-Frequency and Quantum Electronics (IHQ),
University of Karlsruhe, 76131, Karlsruhe, Germany*

***Max-Planck Research Group for Optics, Info. and Photonics
University of Erlangen-Nuremberg, Guenther-Scharowsky-Str. , Germany*

**Graduate School of Science and Engineering,
University of Toyama, Gofuku 3190, Toyama, Japan*

Acknowledgements:

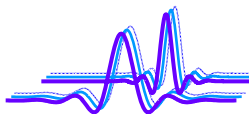
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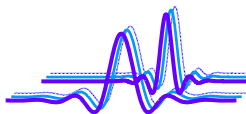
Overview

- **FWM in micro-resonator**

- wavelength conversion, optical switches, etc.
- in a nonlinear resonator: $\chi^{(3)}$ enhanced by $\sim (FE)^8$
- challenging task, numerically & theoretically
- require accurate information on resonance field in complicated stru.
- strong material dispersion of semiconductors

- **Full wave FDTD analysis**

- accurate, but numerically expensive
- efficient parallel code
- detailed modeling capability
 - Kerr nonlinearity
 - material dispersion
 - Effective Dielectric Const. (EDC) tech. for modeling curved surfaces
- first attempt to apply full wave analysis to FWM in actual devices





FDTD analysis of nonlinear and dispersive media

Optical Kerr effect

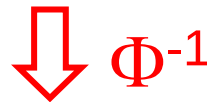
polarization: $P_K(t) = \varepsilon_0 \chi_K^{(3)} E^3(t)$ $\Rightarrow$ finite difference eq.



const. nonlinear susceptibility

Lorentz dispersion

polarization: $\tilde{P}_L(\omega) = \tilde{\chi}_L(\omega) \tilde{E}(\omega) = \frac{\varepsilon_0 \Delta \varepsilon_L \omega_L^2}{\omega_L^2 + 2j\delta_L \omega - \omega^2} \tilde{E}(\omega)$

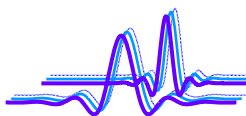


$$\omega_L^2 P_L(t) + 2\delta_L \frac{dP_L(t)}{dt} + \frac{d^2 P_L(t)}{dt^2} = \varepsilon_0 \Delta \varepsilon_L \omega_L^2 E(t)$$

$\Rightarrow$ finite difference eq.

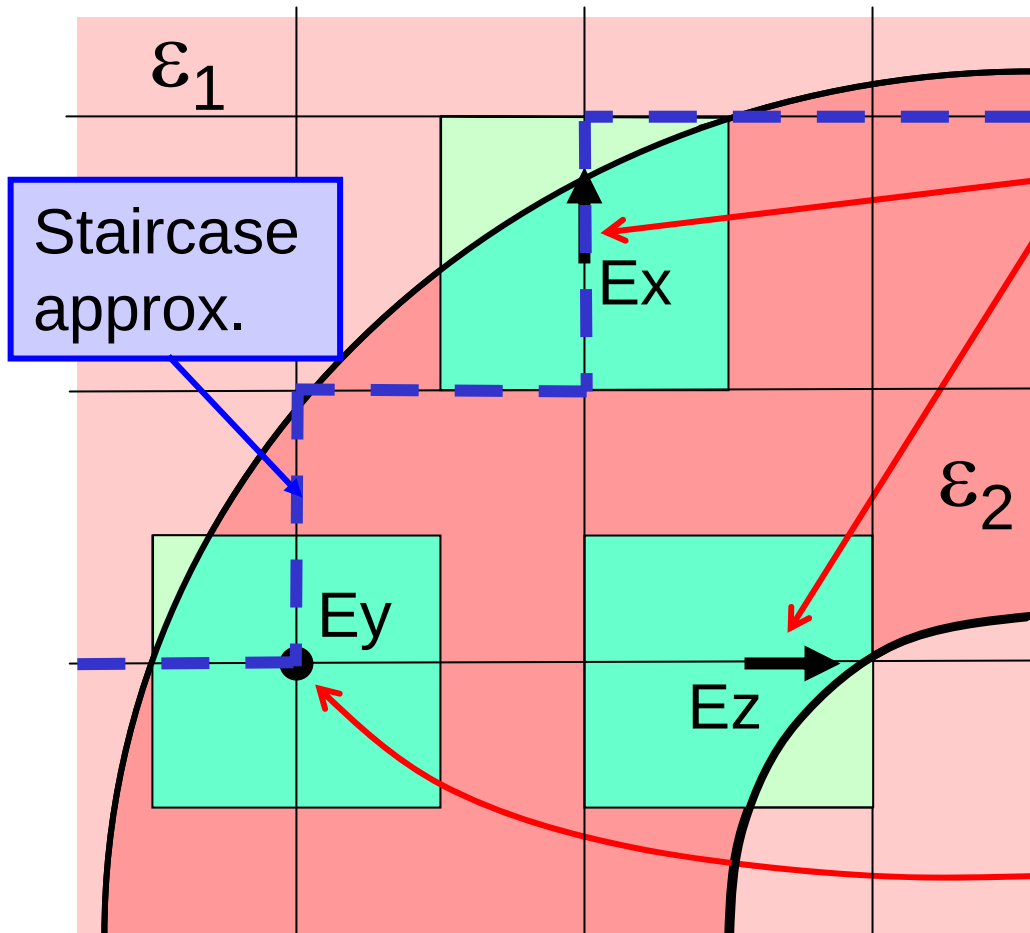


solved in Yee's leapfrog algorithm





FDTD implementation of Effective Dielectric Const. (EDC) Tech.



For E fields not being tangential to the interface:

ϵ_{eff} : solve electrostatic Laplace equation

$$\nabla \cdot (\epsilon \nabla \phi) = 0$$

by FD method

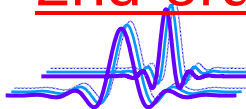
For E fields tangential to the interface:

Tangential B.C.

(E is continuous)

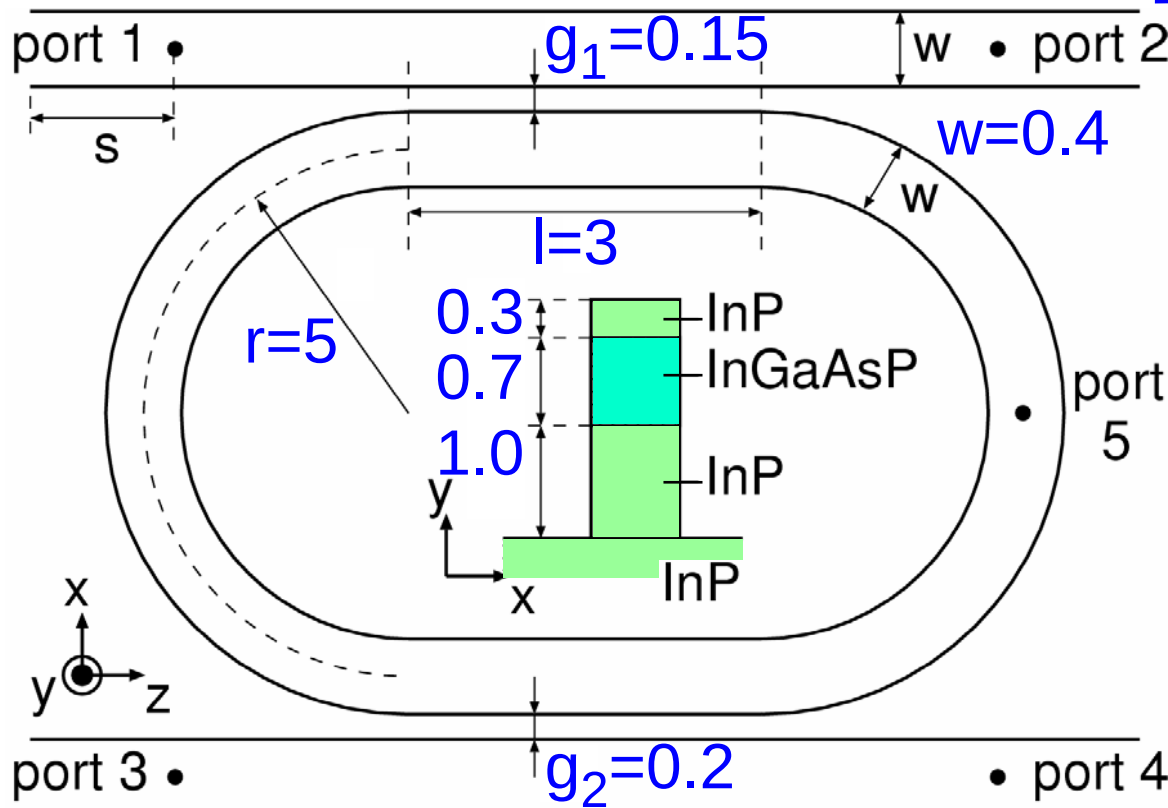
ϵ_{eff} : arithmetic average

2nd-order accuracy is maintained!

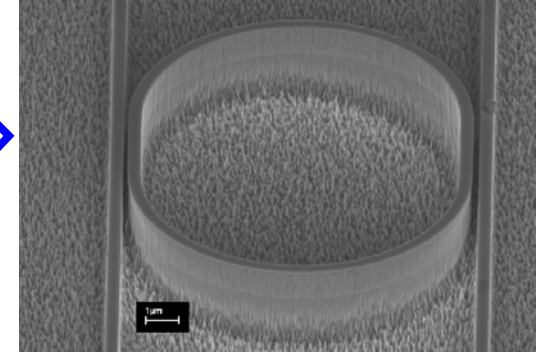


Modeling of InP/InGaAsP micro-resonator

Resonator structure (2D and 3D)



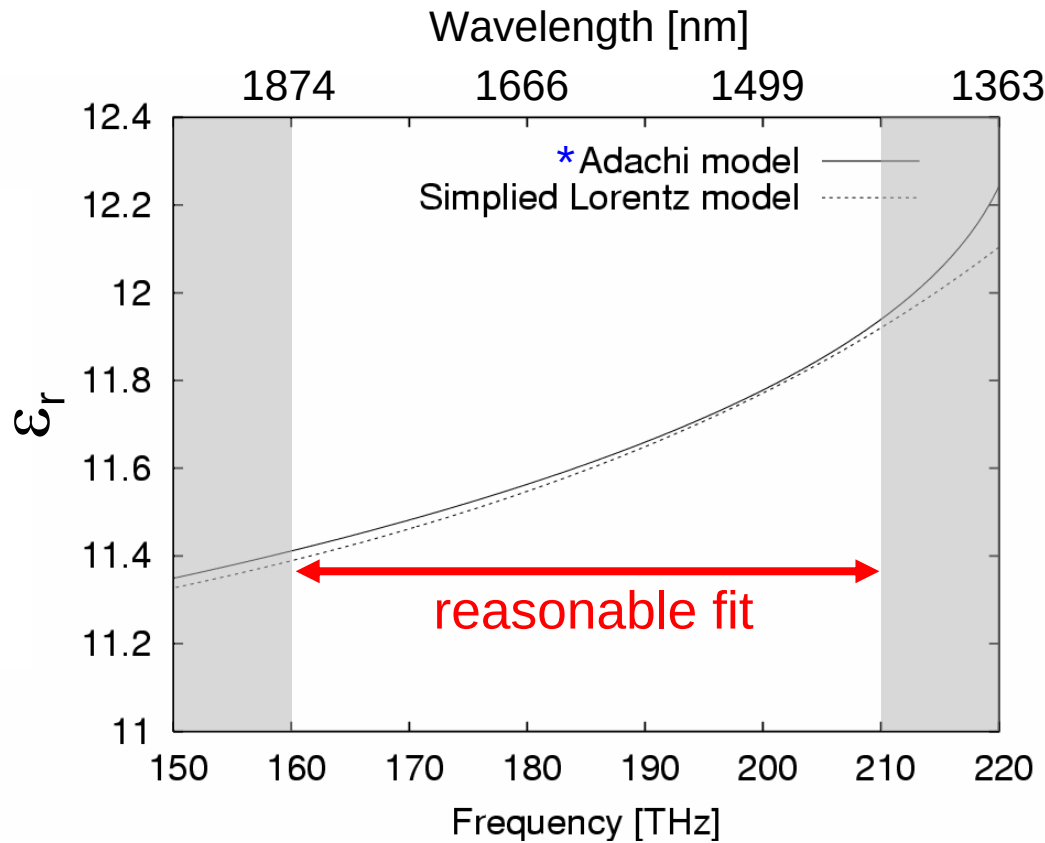
$\Delta x = \Delta z = 0.025$, $\Delta y = 0.1 \mu\text{m}$ (unit: μm)



- substrate: InP
- computation region: $13.5 \times 17.4 \mu\text{m}^2$, for 3D; height = $2.7 \mu\text{m}$
- **InGaAsP**: $n=3.42$
 $\chi^{(3)} = 3.8 \times 10^{18} \text{ m}^2/\text{V}^2$
- **InP**: $n=3.17$ ($1.55 \mu\text{m}$)
- for 2D analysis; $n=3.34$ (slab wg.)
- quasi-TM pol.

Modeling of InP/InGaAsP micro-resonator

Material dispersion of InGaAsP core



dielectric const. for
Q(1.35)-InGaAsP:

$$\varepsilon_r = \varepsilon_\infty + \chi^{(1)} + \chi^{(3)} E^2$$

$$\chi^{(1)} = \frac{\Delta\varepsilon \omega_p^2}{\omega_p^2 - \omega^2}$$

$$\chi^{(3)} = 3.8 \times 10^{18} \text{ m}^2/\text{V}^2$$

with $\varepsilon_{\text{inf}} = 10.05$

$$\Delta\varepsilon = 1.0$$

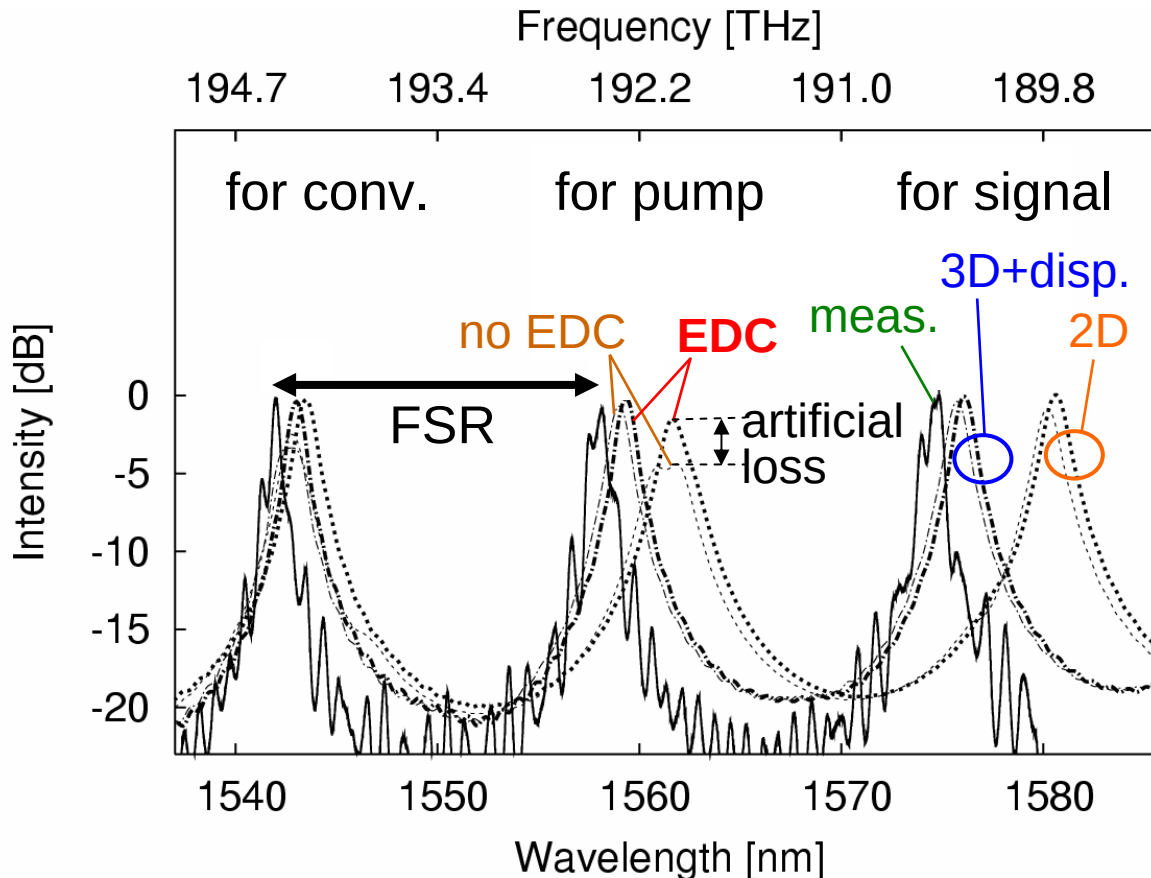
$$\omega_p = 1.948 \times 10^{15}$$

rad/s

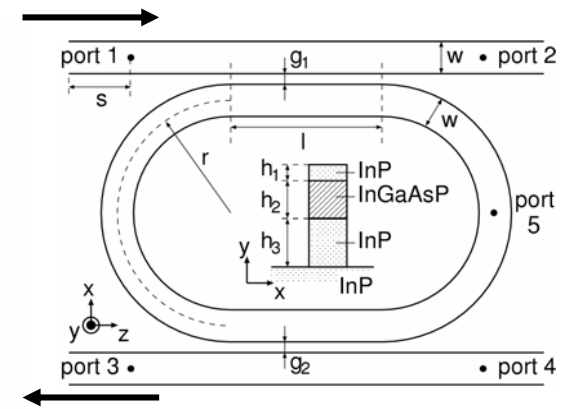
*S. Adachi, "Optical properties of $\text{In}_{1-x}\text{Ga}_x\text{As}_y\text{P}_{1-y}$ alloys",
Phys. Rev. B, vol. 39, no. 17, pp. 12612–12621, 1989.

Modeling of InP/InGaAsP micro-resonator

Linear pulse response analysis



pulse input (quasi-TM)



output

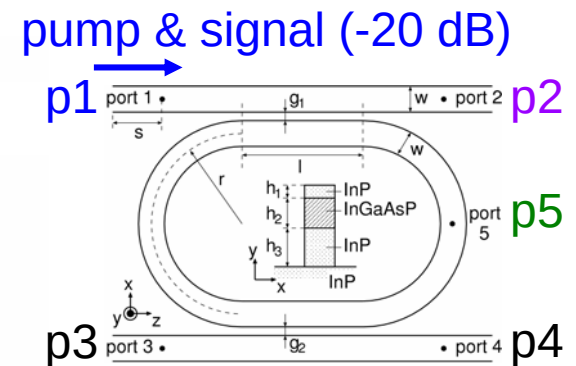
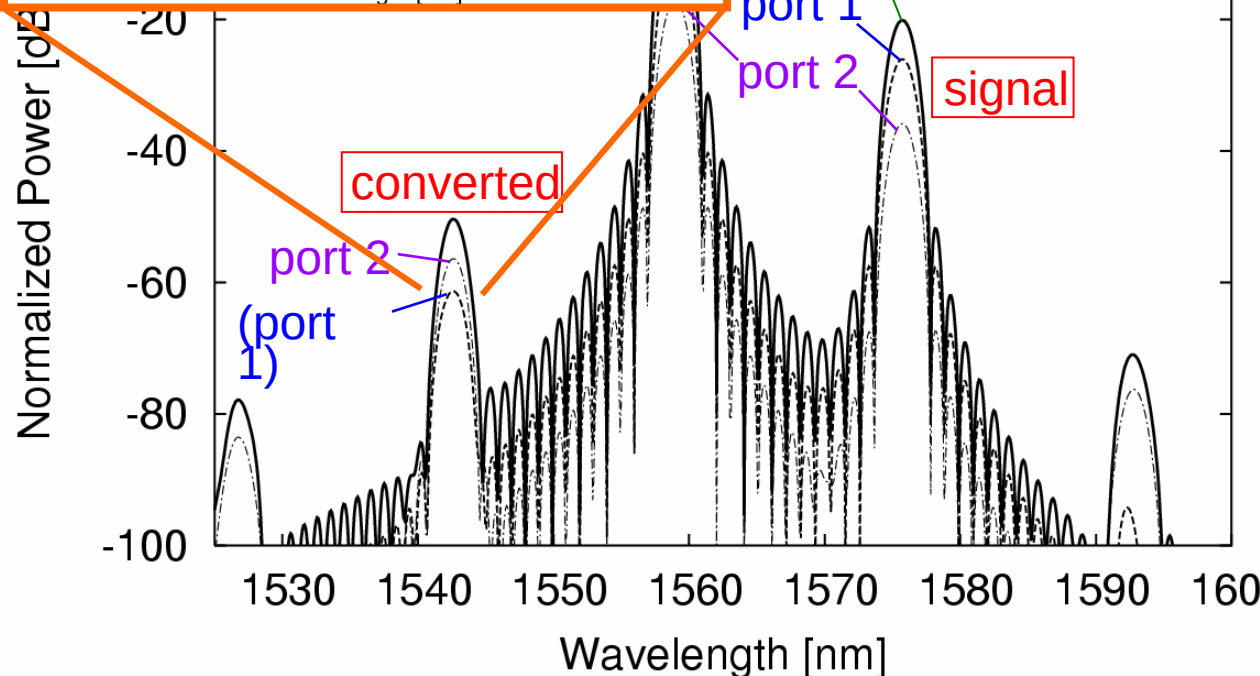
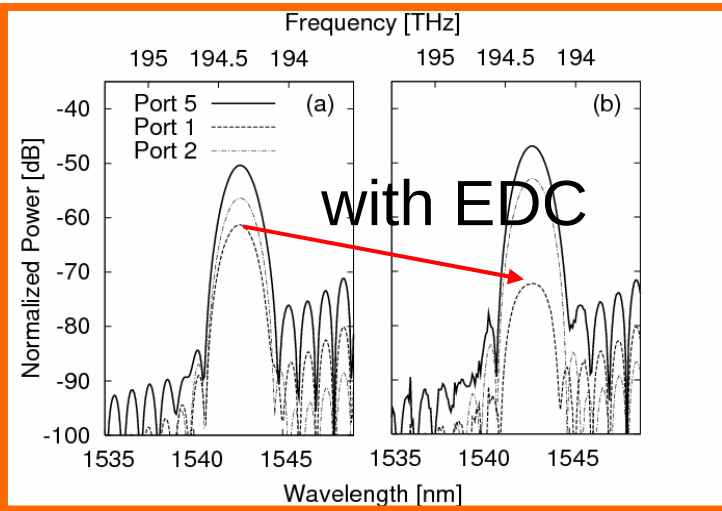
FSR error (FDTD vs. meas.)

2D	2D +disp.	3D	3D +disp.
13 %	4%	10%	1%

- **EDC** reduces stair-case error (artificial loss)

Modeling of InGaAsP micro-resonator

s (typical DFWM spectrum)

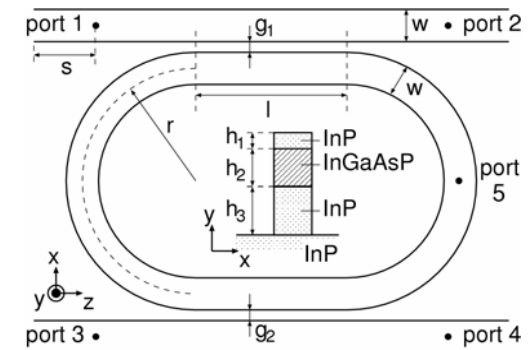
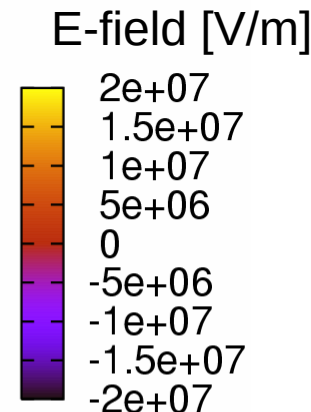
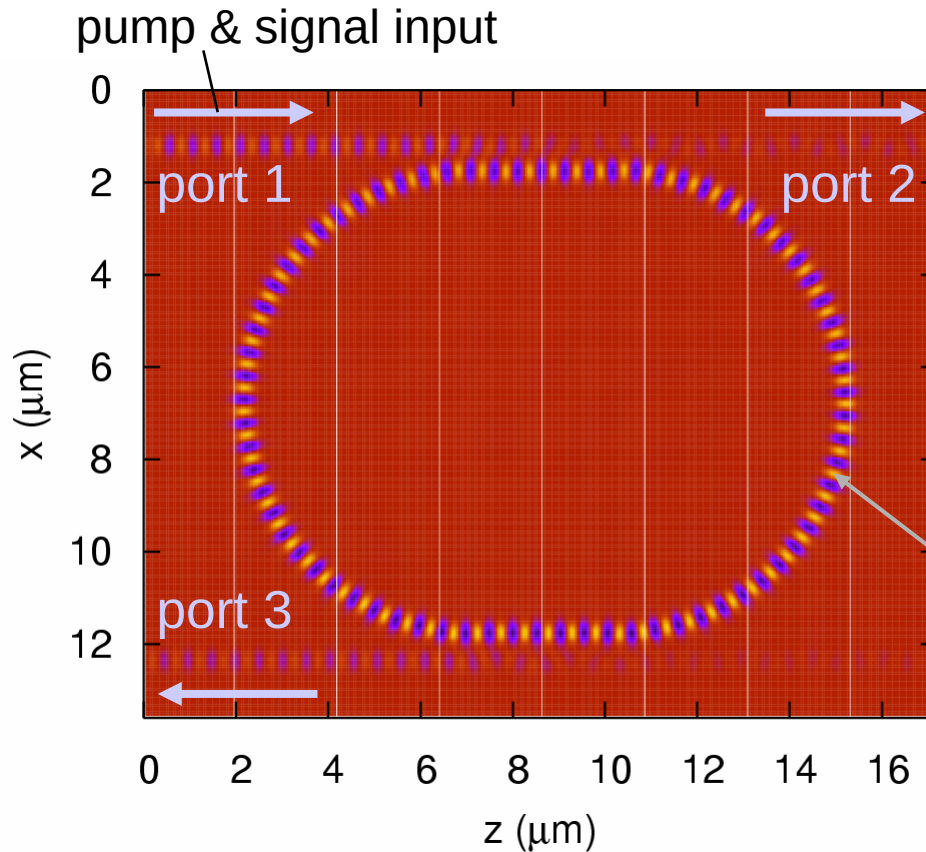


calculation conditions:

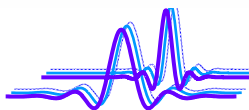
- pump & signal input at p1
- **3D FDTD (max 18 ps)**
- max pump field at center of waveguide:
 $E_p = 5.65 \times 10^6$ V/m
(=pump power 13 dBm)
- material dispersion
- no EDC

Modeling of InP/InGaAsP micro-resonator

Field enhancement in resonator (q-TM E-field)

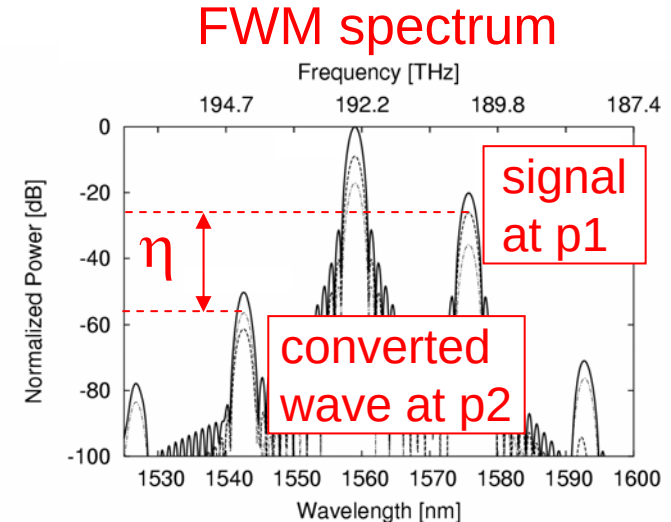
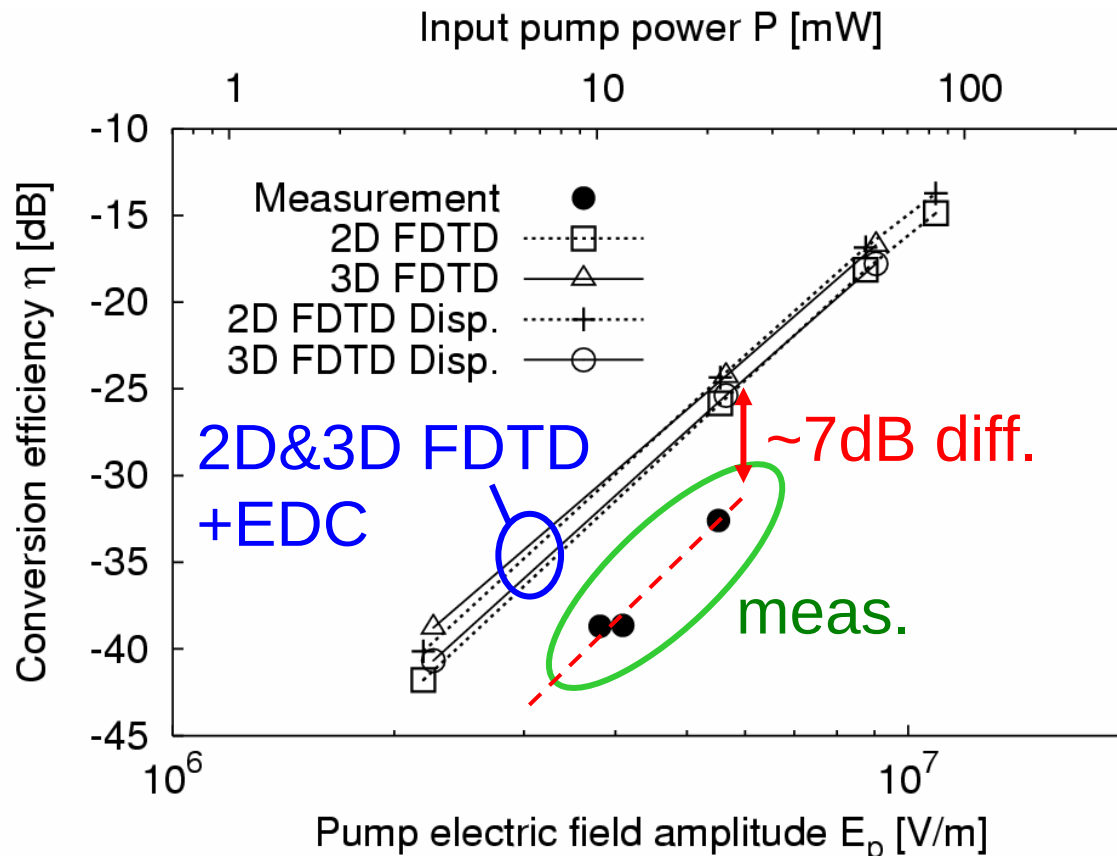


Note:
Field in the ring is much
stronger than that in the
bus waveguides.
FE ~ 2.4



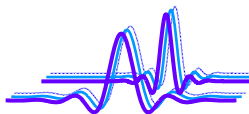
Comparison with measurements

Wavelength conversion efficiencies of FWM



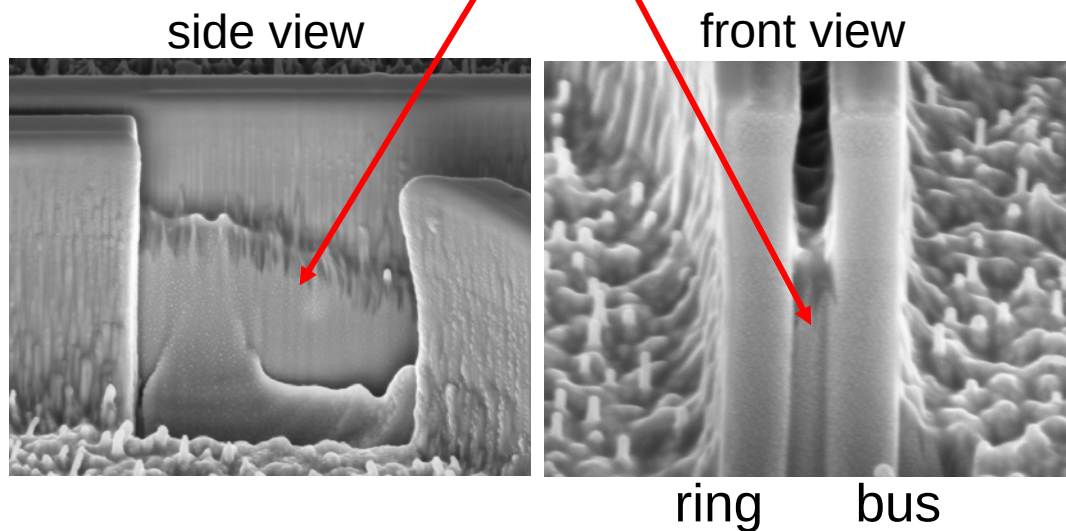
Results:

- 2D, 3D FDTD w/wo disp. agree well.
- FDTD vs. meas. ~7dB difference

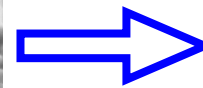


Discussions

- Wavelength conversion efficiencies η of FWM
 - 7dB difference of η between FDTD and measurement
 - **fabrication tolerance** for coupling gap (20% wider)
 $g_1 \sim 0.185 \mu\text{m}$ (nominal 0.15), $g_2 \sim 0.240 \mu\text{m}$ (nom. 0.20)
 - Incompletely etched residual in gaps

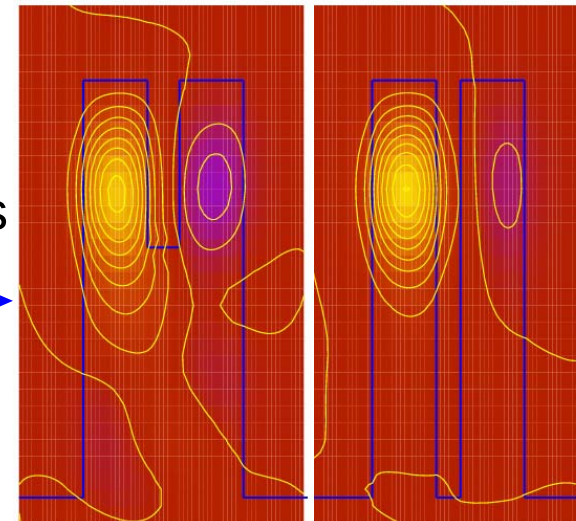


3D
analysis

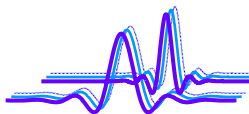


incomplete
etch in gaps

normal
gap



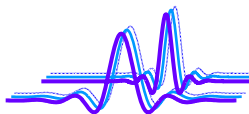
⇒ **significant reduction of η !**





Discussions

- Computational resource
 - 3D FDTD with 64 CPUs (U.Karlsruhe, HP XC-6000)
run time: 28 hours.
total memory: up to approx. 4GB
 - 3D FDTD with 12 CPUs (Dell Poweredge cluster)
run time: 98 hours.
 - 2D FDTD with 32 CPUs (with 3D code, XC-6000)
run time: approx. 150 min
total memory: up to approx. 500MB





Conclusions

- 2D & 3D FDTD analysis of DFWM in micro-resonator
 - optical Kerr nonlinearity
 - material dispersion: Lorentz model incl.
 - efficient stair-case roughness compensation by EDC (Effective Dielectric Constant) Technique
 - parallel computation allows efficient 3D analysis
 - Results:
 - 7dB difference in conversion efficiency, mainly due to fabrication tolerance and incomplete etching in gap region

With full-wave FDTD analysis, it will be possible to show what happens in an actual device, and then what to do next!

